

1 Sinusoids

$$\begin{aligned}\omega &= 2\pi f & f &= T^{-1} & \theta &= \omega t + \phi \\ z &= x + jy = Ae^{j\theta} = A \cos \theta + jA \sin \theta = A \angle \phi^\circ \\ x + jy: x &= A \cos \theta & y &= A \sin \theta & \theta &= \tan^{-1} \frac{y}{x} & A &= \sqrt{x^2 + y^2} \\ \frac{A_1 \angle \phi_1^\circ}{A_2 \angle \phi_2^\circ} &= \frac{A_1}{A_2} \angle (\phi_1 - \phi_2)^\circ & A_1 \angle \phi_1^\circ \cdot A_2 \angle \phi_2^\circ &= A_1 \cdot A_2 \angle (\phi_1 + \phi_2)^\circ \\ A \cos(\omega t) &= A \sin(\omega t + \frac{\pi}{2}) & A \sin(\omega t) &= A \cos(\omega t - \frac{\pi}{2}) \\ y_{\max} &= A & y_{\text{rms}} &= \frac{y_{\max}}{\sqrt{2}} & y_{\text{rms}} &= \sqrt{\frac{1}{T} \int_0^T [y(t)]^2 dt}\end{aligned}$$

2 Circuit Basics and Definitions

$$\begin{aligned}V &= RI & P &= VI = RI^2 = \frac{V^2}{R} & E(t) &= \int p(t) dt \\ i &= \frac{dq}{dt} & \sum I_{\text{node}} &= 0 & V &= \frac{dE_p}{dq} & \sum V_{\text{loop}} &= 0 \\ \rho &= R \frac{A}{\ell} [\Omega \text{ m}] & \sigma &= \frac{\ell}{RA} [\text{S m}^{-1}] & J &= \frac{I}{A}\end{aligned}$$

2.1 Resistance

$$\begin{aligned}R_{\text{series}} &= \sum_i R_i & R_{\text{parallel}} &= [\sum_i (R_i^{-1})]^{-1} & R_{\text{parallel}} &= \frac{R_1 R_2}{R_1 + R_2} \\ V_0, R_{\text{series}}: V_i &= \frac{R_i}{R_{\text{series}}} V_0 & I_0, R_{\text{parallel}}: I_i &= \frac{R_{\text{parallel}}}{R_i} I_0 \\ i_R(t) &= \frac{V_{\max}}{R} \sin(\omega t + \phi) & v_R(t) &= V_{\max} \sin(\omega t + \phi) \\ V_{\max} e^{j\phi} &= RI_{\max} e^{j\phi} & \bar{V} &= RI_{\max} \angle \phi^\circ\end{aligned}$$

2.2 Capacitance

$$\begin{aligned}C &= \frac{q}{V} & E_C(t) &= \frac{1}{2} C v_C(t)^2 & C_{\text{plates}} &= \epsilon_0 \epsilon_R \frac{A}{\delta} \\ C_{\text{parallel}} &= \sum_i C_i & C_{\text{series}} &= [\sum_i (C_i^{-1})]^{-1} \\ V_{\max} &= X_C I_{\max} & X_C &= \frac{1}{\omega C} & C &= \frac{I_C^2}{\omega Q_C} \\ i_C &= C \frac{dv_C}{dt} & v_C(t) &= v_{C0} + \frac{1}{C} \int_0^t i_C(t') dt' \\ I_{\max} e^{j\phi_I} &= j\omega C V_{\max} e^{j\phi_V} & \bar{I} &= \omega C [V_{\max} \angle (\phi_V + 90)^\circ]\end{aligned}$$

2.3 Inductance

$$\begin{aligned}L &= \frac{\Phi_B}{I} & E_L(t) &= \frac{1}{2} L i_L(t)^2 & L_{\text{coil}} &= \frac{N_t \Phi_B}{I} = \frac{\lambda}{I} \approx \frac{\mu_0 N_t^2 A \sigma}{\ell} \\ L_{\text{series}} &= \sum_i L_i & L_{\text{parallel}} &= [\sum_i (L_i^{-1})]^{-1} \\ V_{\max} &= X_L I_{\max} & X_L &= \omega L & L &= \frac{f_0 R}{\omega} & L &= \frac{Q_L}{I_L^2 \omega} \\ v_L(t) &= L \frac{di_L}{dt} & i_L(t) &= i_{L0} + \frac{1}{L} \int_0^t v_L(t') dt' \\ V_{\max} e^{j\phi_V} &= j\omega L I_{\max} e^{j\phi_I} & \bar{V} &= \omega L [I_{\max} \angle (\phi_I + 90)^\circ]\end{aligned}$$

2.4 Impedance and Reactance

$$\begin{aligned}Z &= R + jX & |Z| &= \sqrt{R^2 + X^2} & X &= X_L - X_C \\ Z_{\text{series}} &= \sum_i Z_i & Z_{\text{parallel}} &= [\sum_i (Z_i^{-1})]^{-1} \\ Z \angle \phi^\circ: \phi &= \tan^{-1} \frac{X}{R} & R &= |Z| \cos \phi & X &= |Z| \sin \phi \\ \bar{Z}_R &= R \angle 0^\circ = R \\ \bar{Z}_C &= \frac{1}{\omega C} \angle -90^\circ = X_C \angle -90^\circ & Z_C &= \frac{1}{j\omega C} & X_C &= \frac{1}{\omega C} \\ \bar{Z}_L &= \omega L \angle +90^\circ = X_L \angle +90^\circ & Z_L &= j\omega L & X_L &= \omega L\end{aligned}$$

2.5 Admittance, Conductance, and Susceptance

$$\begin{aligned}Y &= G + jB = \frac{1}{Z} = \frac{I}{V} & Y_{\text{parallel}} &= \sum_i Y_i & Y_{\text{series}} &= [\sum_i (Y_i^{-1})]^{-1} \\ G &= R^{-1} & B &= \frac{1}{X} & B_C &= \omega C & B_L &= -\frac{1}{\omega L}\end{aligned}$$

2.5.1 Y Bus Matrix

$$\begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_n \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} & \cdots & y_{1n} \\ y_{21} & y_{22} & \cdots & y_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ y_{n1} & y_{n2} & \cdots & y_{nn} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_n \end{bmatrix}$$

$y_{ii} = \sum_n Y_n$ (into node) $y_{ij} = \sum_n -Y_n$ (directly between nodes)

3 Power

3.1 Average Power

$$\begin{aligned}p &= vi = \frac{1}{2} V_{\max} I_{\max} [\cos(\phi_V - \phi_I) + \cos(2\omega t + \phi_V + \phi_I)] \\ \langle p \rangle &= \frac{1}{T} \int_0^T p(t) dt = \frac{1}{2} V_{\max} I_{\max} \cos(\phi_V - \phi_I) = \frac{RI_{\max}^2}{2} = \frac{V_{\max}^2}{2R}\end{aligned}$$

3.2 Complex Power, Single Phase

$$\begin{aligned}\bar{V}_{\text{rms}} &= \bar{Z} \bar{I}_{\text{rms}} & \phi &= \phi_V - \phi_I & \theta_{\text{pf}} &= \phi \\ S &= \frac{1}{2} V_{\max} I_{\max}^* = \bar{V}_{\text{rms}} \bar{I}_{\text{rms}}^* = |\bar{I}_{\text{rms}}|^2 \bar{Z} = \frac{|\bar{V}_{\text{rms}}|^2}{\bar{Z}^*} \\ S &= P \pm jQ & P &= \Re(S) & Q &= \Im(S) & |S| &= \sqrt{P^2 + Q^2} \\ P &= \bar{V}_{\text{rms}} \bar{I}_{\text{rms}} \cos \phi = |\bar{I}_{\text{rms}}|^2 R = \frac{|\bar{V}_{\text{rms}}|^2}{|\bar{Z}|^2} R = |S| \cos \phi = \frac{|\bar{V}_{\text{rms}}|^2 \cos \phi}{|\bar{Z}|} \\ Q &= \bar{V}_{\text{rms}} \bar{I}_{\text{rms}} \sin \phi = |\bar{I}_{\text{rms}}|^2 \bar{X} = \frac{|\bar{V}_{\text{rms}}|^2}{|\bar{Z}|^2} \bar{X} = |S| \sin \phi = \frac{|\bar{V}_{\text{rms}}|^2 \sin \phi}{|\bar{Z}|} \\ \text{pf} &\equiv \frac{P}{|\bar{V}_{\text{rms}}| |\bar{I}_{\text{rms}}|} = \frac{P}{|S|} = \cos \phi = R / \sqrt{R^2 + X^2} \\ \{\theta_{\text{pf}} > 0\} &: (\text{ind, lag, } +Q) & \{\theta_{\text{pf}} < 0\} &: (\text{cap, lead, } -Q) \\ \text{Purely resistive: } P &= \frac{|V|^2}{R} & \text{Purely reactive: } Q &= \frac{|V|^2}{X} \\ \text{pf correction: } C &= \frac{Q_{\phi 2} - Q_{\phi 1}}{-|\bar{V}_{\phi, \text{rms}}|^2 \omega} & L &= \frac{-|V_{\phi, \text{rms}}|^2}{\omega(Q_{\phi 2} - Q_{\phi 1})} \\ \{\bar{Z}_{\text{Ld}} = \bar{Z}_S^*\} &\Leftrightarrow \{P = P_{\max}\}\end{aligned}$$

3.3 Complex Power, 3 Phase

Notation: $V_{\alpha\beta} : \alpha > \beta$ $I_{\alpha\beta} : \alpha \rightarrow \beta$ X : source x : load

$$\begin{aligned}S_T &= \sum S_\phi = |\bar{V}_{\text{Ln}}| |\bar{I}_{\text{Ln}}| \cdot \sqrt{3} \angle \phi_Z^\circ \\ |\bar{I}_{\text{Ln}}| &= |\bar{I}_{\text{an}}| = |\bar{I}_{\text{nb}}| = |\bar{I}_{\text{nc}}| \\ |\bar{V}_{\text{Ln}}| &= |\bar{V}_{\text{ab}}| = |\bar{V}_{\text{bc}}| = |\bar{V}_{\text{ca}}| \\ \bar{Z}_\Delta &= 3\bar{Z}_Y & \Delta\phi &= 120^\circ \\ \bar{V}_{\Delta, AB} &= \bar{V}_{Y, AN} \cdot \sqrt{3} \angle 30^\circ\end{aligned}$$

3.3.1 Y Source / Y Load

$$\begin{aligned}\bar{V}_{\text{Ln}} &= \bar{V}_\phi \cdot \sqrt{3} \angle 30^\circ \\ \bar{V}_{AB} &= \bar{V}_{AN} - \bar{V}_{BN} = \bar{V}_{AN} \cdot \sqrt{3} \angle 30^\circ & \sum_i \bar{V}_{iN} &= 0 \\ \text{Y-Y: } \bar{I}_{\text{an}} &= \frac{\bar{V}_{AN}}{Z_Y + Z_{\text{Ln}}} & S_{\phi a} &= \bar{V}_{\text{an}} \bar{I}_{\text{an}}^* & \bar{V}_{\text{an}} &= \bar{I}_{\text{Ln}} \bar{Z}_Y\end{aligned}$$

3.3.2 Δ Source / Δ Load

$$\begin{aligned}\bar{I}_{\text{Ln}} &= \bar{I}_\phi \cdot \sqrt{3} \angle -30^\circ \\ \bar{I}_{Aa} &= \bar{I}_{ab} - \bar{I}_{ca} = \bar{I}_{ab} \cdot \sqrt{3} \angle -30^\circ & \sum \bar{I}_{\text{node}} &= 0 \\ \Delta\text{-}\Delta: \bar{I}_{ab} &= \frac{\bar{V}_{AB}}{\bar{Z}_\Delta} & S_{\phi a} &= \bar{V}_{AB} \bar{I}_{ab}^*\end{aligned}$$

3.3.3 Y Source / Δ Load

$$\begin{aligned}\bar{V}_{ab} &= \bar{V}_{AB} = \bar{V}_{AN} \cdot \sqrt{3} \angle 30^\circ \\ \bar{I}_{ab} &= \frac{\bar{V}_{AB}}{\bar{Z}_\Delta} & \bar{I}_{Aa} &= \bar{I}_{ab} \cdot \sqrt{3} \angle -30^\circ \\ S_{\phi a} &= \bar{V}_{AB} \bar{I}_{ab}^* = (\bar{V}_{AN} \cdot \sqrt{3} \angle 30^\circ) \bar{I}_{ab}^*\end{aligned}$$

4 Magnetically Coupled Circuits

$$\begin{aligned}\vec{F}_{\text{surfaces}} &= \frac{\vec{B}^2 A}{2\mu_0} & \vec{\mathcal{F}} &= N_t I = \Phi_B \mathcal{R} & |\Phi| &\propto |I| \\ \mathcal{R} &= \frac{\ell}{\mu A} & \mu &= \mu_0 \mu_R & \vec{B} &= \frac{\Phi_B}{A} = \frac{\mu \vec{\mathcal{F}}}{\ell} = \mu \vec{H} \\ \mu_0 &= 4\pi \text{E-}7 \frac{\text{H}}{\text{m}} & \epsilon_0 &= 8.854 \text{E-}12 \frac{\text{F}}{\text{m}} & c_0 &= (\mu_0 \epsilon_0)^{-\frac{1}{2}}\end{aligned}$$

4.1 1 Phase Ideal Transformers

$$\begin{aligned}v_i &= N_{t,i} \frac{d\Phi_{B,i}}{dt} & V_1 I_1 &= V_2 I_2 \\ \{\Phi_{B1} = \Phi_{B2}\}: \frac{V_1}{V_2} &= \frac{N_{t,1}}{N_{t,2}} = a & \frac{I_1}{I_2} &= \frac{N_{t,2}}{N_{t,1}} = \frac{1}{a} \\ V_1 &= a V_2 & I_1 &= \frac{I_2}{a} & Z_1 &= a^2 Z_2 \\ 1: \text{source} & 2: \text{load} & \{a > 1\}: \text{step-down} & \{a < 1\}: \text{step-up} \\ \Phi_B(t) &= A_\Phi \sin \omega t & v &= 2\pi f N_t A_\Phi \cos \omega t & A_\Phi &\equiv \Phi_{B, \max} \\ V_{\max} &= 2\pi f N_t A_\Phi & V_{\text{rms}} &= \frac{2\pi}{\sqrt{2}} f N_t A_\Phi \\ S_{\text{rated}} &= V_{\text{rated}} I & A_{\sigma, \min} &= \frac{A_\Phi}{\bar{B}_{\text{material}}}\end{aligned}$$

4.2 1 Phase Real Transformers

$$\begin{aligned}\bar{V}_1 &= \bar{a} \bar{V}_2 = |\bar{a}| |\bar{V}_2| \angle (\phi_{V2} + \phi_a)^\circ & \bar{I}_1 &= \frac{\bar{I}_2}{\bar{a}^*} & \bar{Z}_1 &= |\bar{a}|^2 \bar{Z}_2 \\ \hat{P}_e &= k_e f^2 \bar{B}_{\max}^2 \delta^2 & \hat{P}_h &= k_h f \bar{B}_{\max}^{\text{ns}}\end{aligned}$$

4.2.1 SC-OC Test

$$\begin{aligned}Z_{\text{eq1}} &= \frac{V_{\text{sc}}}{I_{\text{sc}}} = R_{\text{eq1}} + jX_{\text{eq1}} & R_{\text{eq1}} &= \frac{P_{\text{sc}}}{I_{\text{sc}}^2} & X_{\text{eq1}} &= \sqrt{Z_{\text{eq1}}^2 - R_{\text{eq1}}^2} \\ \phi &= \cos^{-1} \frac{P_{\text{oc}}}{I_{\text{oc}} V_{\text{oc}}} & I_c &= I_{\text{oc}} \cos \phi & I_m &= I_{\text{oc}} \sin \phi \\ R_{\text{core2}} &= \frac{V_{\text{oc}}}{I_{\text{core}}} & X_{\text{mutual2}} &= \frac{V_{\text{oc}}}{I_{\text{mutual}}} & R_{\text{eq2}} &= \frac{R_{\text{eq1}}}{a^2} & X_{\text{eq2}} &= \frac{X_{\text{eq1}}}{a^2}\end{aligned}$$

$$x = \frac{S_{Ld}}{S_{rated}} \quad \eta \equiv \frac{x \cdot S_{rated} \cdot pf}{x \cdot S_{rated} \cdot pf + \underbrace{P_{OC}}_{P_{core}} + x^2 \underbrace{P_{sc}}_{P_{Cu FL}}} \quad \{x^2 P_{Cu FL} = P_{core}\} : \eta_{max}$$

4.2.2 Voltage Regulation

$$\frac{V_1}{a} = \bar{V}_{Ld} + \bar{I}_{Ld}(R_{eq2} + jX_{eq2})$$

$$V_{R,NL} = \frac{|V_1|}{a} \quad V_{R,FL} = |V_{rated}| \quad VR = \frac{V_{R,NL} - V_{R,FL}}{V_{R,FL}} \times 100\%$$

$$\frac{V_1}{a} = \sqrt{(|\bar{V}_{Ld}| \cos \phi + |\bar{I}_{Ld}| R_{eq2})^2 + (|\bar{V}_{Ld}| \sin \phi \pm |\bar{I}_{Ld}| X_{eq2})^2}$$

(+) lagging, unity (-) leading

5 Per Unit System

$$F \in \{V, I, R, Z, X, S\} : \dot{F} \cdot F_b = F_{actual}$$

$$S_b = \bar{V}_b \bar{I}_b^* \quad \bar{Z}_b = \frac{\bar{V}_b^2}{S_b} \quad \dot{S} = \dot{P} \pm j\dot{Q} = \dot{V} \dot{I}^*$$

$$\bar{Z}_{b,i} = \frac{\bar{V}_{b,i}^2}{S_b} \quad \bar{I}_{b,i} = \frac{S_b}{\bar{V}_{b,i}} \quad \bar{V}_{b,i} = \bar{V}_{b,0} \frac{V_{i,0}}{V_0} \quad [HV \text{ or } LV \text{ basis}]$$

5.1 Lossy Transformer

$$\eta \equiv \frac{x \cdot pf}{x \cdot pf + \frac{P_{core}}{S_b} + x^2 R} \quad \dot{R} = \dot{P}_{Cu FL} = \frac{P_{Cu FL}}{S_b} = \frac{R_{eq1}}{Z_{b1}} = \frac{R_{eq2}}{Z_{b2}}$$

5.2 3 Phase Power

$$\bar{V}_{b,AN} = \frac{\bar{V}_{b,AB}}{\sqrt{3}} \quad |S_T| = \sqrt{3} |V_{AB}| |I_{Aa}|$$

$$I_{b,3\phi} = \frac{S_{b,3\phi}}{\sqrt{3} V_{b,3\phi,AB}} = \frac{S_{b,1\phi}}{V_{b,1\phi}} \quad Z_{b,3\phi} = \frac{V_{b,3\phi,AB}^2}{S_{b,3\phi}}$$

5.3 Tertiary Transformer Star Equivalent Circuit

1 excited, 2 shorted: $\frac{V}{I} = Z_{12}$ 1 excited, 3 shorted: $\frac{V}{I} = Z_{13}$

2 excited, 3 shorted: $\frac{V}{I} = Z_{23, sec.}$ $Z_{23, primary} = \left(\frac{N_{1,1}}{N_{1,2}}\right)^2 Z_{23, sec.}$

$$X_1 = \frac{1}{2}(Z_{12} + Z_{13} - Z_{23}) \quad X_2 = \frac{1}{2}(Z_{12} + Z_{23} - Z_{13})$$

$$X_3 = \frac{1}{2}(Z_{13} + Z_{23} - Z_{12})$$

$$Z_{b,1} = \frac{V_{b,1}}{S_b} \quad \dot{Z}_1 = \frac{jX_1}{Z_{b,1}} \quad \dot{Z}_2 = \frac{jX_2}{Z_{b,1}} \quad \dot{Z}_3 = \frac{jX_3}{Z_{b,1}}$$

5.4 Off Nominal Turns Ratio, Pi Equivalent

Transformer nameplate: $\dot{Z}'_i = \dot{Z}_i \left(\frac{V_{b,i}}{V_{b,0}}\right)^2 \frac{S'_{b,0}}{S_{b,i}}$ [b, 0 in basis zone]

$$Z_{T,HV} = c^2 Z_{T,LV} \quad c \equiv \sqrt{\frac{\dot{Z}'_{T,HV}}{\dot{Z}'_{T,LV}}} \quad Y_{eq} = (\dot{Z}'_{T,HV})^{-1}$$

$$Y_{10} = (1 - c)Y_{eq,HV} \quad Y_{12} = cY_{eq} \quad Y_{20} = (|c|^2 - c)Y_{eq}$$

6 Transmission

$$A [CM] = (\varnothing [\text{mil}])^2 \quad 1 \text{ mil} = 0.001 \text{ in} \quad 1 \text{ CM} = 5.066 \times 10^{-10} \text{ m}^2$$

$$R = \frac{\rho(T) \ell}{A_{\sigma,T}} \quad \rho(T_2) = \rho(T_1) \frac{M+T_2}{M+T_1}$$

$$\bar{\delta}_{m \times n} = \sqrt[m \cdot n]{\prod_{i=1}^m \prod_{j=1}^n \delta(m_i, n_j)}$$

$$\bar{R}_L = \sqrt[n]{\prod_{i=1}^n \prod_{j=1}^n \delta_{ij}} \quad \delta_{i=j} \equiv e^{-0.25} R_{wire}$$

$$\bar{R}_C = \sqrt[n]{\prod_{i=1}^n \prod_{j=1}^n \delta_{ij}} \quad \delta_{i=j} \equiv R_{wire}$$

$$\bar{X}_L = \omega \bar{L} \quad \bar{Y} = \omega \bar{C} \quad \bar{Z} = \bar{R} + j\bar{X}$$

6.1 Inductance

$$\tilde{\lambda}_{int} = \frac{\mu_0 I}{8\pi} \quad \tilde{L}_{int} = \frac{\mu_0}{8\pi} \quad \tilde{\lambda}_{ext} = \frac{\mu I}{2\pi} \ln \frac{\bar{\delta}}{R_{wire}} \quad \tilde{L}_{ext} = \frac{\mu_0}{2\pi} \ln \frac{\bar{\delta}}{R_{wire}}$$

$$\tilde{L}_{line} = 2E-7 \frac{H}{m} \ln \frac{\bar{\delta}}{\bar{R}_L}$$

Single phase, 2 solid conductors:

$$\tilde{L}_{loop} = L_1 + L_2 = 4E-7 \frac{H}{m} \ln \frac{\delta(12)}{\sqrt[2]{e^{-0.5} R_1 R_2}}$$

3 phase, symmetrically spaced solid conductors:

$$\tilde{L}_{\phi} = \frac{\tilde{\lambda}_{\phi}}{I_{\phi}} \quad \tilde{\lambda}_{\phi} = 2E-7 \frac{H}{m} I_{\phi} \ln \frac{\delta(12)}{\bar{R}_L} \quad \bar{R}_L = e^{-0.25} R_{wire}$$

Bundled conductors: $\bar{R}_L = \sqrt[n]{\prod_{i=1}^n \delta_{1i}}$

$$3\phi \text{ transpose: } \tilde{L}_{\phi} = 2E-7 \frac{H}{m} \ln \frac{\sqrt[3]{\delta(12)\delta(23)\delta(31)}}{\bar{R}_L}$$

6.2 Capacitance

Single phase, 2 solid conductors:

$$C_{AB} = \frac{q}{V_{AB}} \quad C_{AN} = \frac{q}{\frac{1}{2} V_{AB}}$$

$$\tilde{C}_{AN} = 2\pi\epsilon_0 \left(\ln \frac{\bar{\delta}}{\bar{R}_C}\right)^{-1}$$

$$3\phi \text{ transpose: } \tilde{C}_{AN} = 2\pi\epsilon_0 \left(\ln \frac{\sqrt[3]{\delta(12)\delta(23)\delta(31)}}{\bar{R}_C}\right)^{-1}$$

$$\tilde{C}_{A\phi} = 2\pi\epsilon_0 \left(\ln \frac{\bar{\delta}}{\bar{R}_C} - \ln \frac{\sqrt[3]{\delta(AB')\delta(BC')\delta(CA')}}{\sqrt[3]{\delta(AA')\delta(BB')\delta(CC')}}\right)^{-1}$$

$$I_{charging} = YV_{AN} = j2\pi f C_{AN} V_{AN}$$

$$Q_{charging,\phi} = YV_{AN}^2 = \omega C_{AN} V_{AN}^2$$

$$Q_{charging,T} = 3YV_{AN}^2 = 3\omega C_{AN} V_{AN}^2 = \omega C_{AN} V_{AB}^2$$

6.3 Distributed Line

$$\begin{bmatrix} \dot{V}_S \\ \dot{I}_S \end{bmatrix} = \underbrace{\begin{bmatrix} A & B \\ C & D \end{bmatrix}}_T \begin{bmatrix} \dot{V}_R \\ \dot{I}_R \end{bmatrix} \quad \dot{V}_S = A\dot{V}_R + B\dot{I}_R$$

$$\dot{I}_S = C\dot{V}_R + D\dot{I}_R$$

$$\gamma \equiv \alpha + j\beta = \sqrt{ZY} [\text{m}^{-1}] \quad Z_0 = \sqrt{\frac{Z}{Y}} [\Omega] \quad A, D [=] \text{pu}$$

6.3.1 Exact Pi (>250 km)

$$T = \begin{bmatrix} \cosh \gamma \ell & Z_0 \sinh \gamma \ell \\ \frac{1}{Z_0} \sinh \gamma \ell & \cosh \gamma \ell \end{bmatrix} \quad \frac{Y_E}{2} = \frac{1}{Z_0} \tanh \frac{\gamma \ell}{2}$$

6.3.2 Nominal Pi (80 km to 250 km)

$$T = \begin{bmatrix} 1 + \frac{Z_N Y_N}{2} & Z_N \\ Y_N \left(1 + \frac{Z_N Y_N}{4}\right) & 1 + \frac{Z_N Y_N}{2} \end{bmatrix} \quad \begin{matrix} Z_N = \ell Z \\ Y_N = \ell Y \end{matrix}$$

6.3.3 Short Line (<80 km)

$$T = \begin{bmatrix} 1 & Z_S \\ 0 & 1 \end{bmatrix} \quad \begin{matrix} Z_S = \ell Z \\ \frac{Y_S}{2} = 0 \end{matrix}$$

6.3.4 Lossless Line

$$Z_0 = \sqrt{\frac{L}{C}} \Omega \quad \gamma = j\omega \sqrt{LC} \text{m}^{-1} \quad \lambda = \frac{1}{f\sqrt{LC}}$$

$$T(x) = \begin{bmatrix} \cosh \gamma x & jZ_0 \sinh \gamma x \\ \frac{1}{Z_0} \sinh \gamma x & \cosh \gamma x \end{bmatrix} \quad \begin{matrix} Z_L = jX_L \\ \frac{Y_L}{2} = \ell \frac{j\omega C_L}{2} \end{matrix}$$

$$\text{SIL} : I_R = \frac{|V_R|}{Z_0} \quad S(x) = V(x)I^*(x) = \frac{|V_R|^2}{Z_0} = \frac{V_{rated}^2}{Z_0}$$

6.3.5 Steady State Stability Limit

$$P_R = \frac{|V_R||V_S|}{|X_L|} \sin(\phi_{V,S} - \phi_{V,R}) = \dot{V}_R \dot{V}_S \cdot \text{SIL} \cdot \frac{\sin(\phi_{V,S} - \phi_{V,R})}{\sin\left(\frac{2\pi\ell}{\lambda}\right)}$$

6.3.6 Maximum Power Flow

$$|A| \angle \phi_A^\circ \equiv T(A) \quad |B| \angle \phi_B^\circ \equiv T(B)$$

$$S_R = \frac{|V_R||V_S|}{|B|} \angle(\phi_B - \phi_{V,S} - \phi_{V,R})^\circ + \frac{|V_R|^2 |A|}{|B|} \angle(\phi_B - \phi_A - 180)^\circ$$

References

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